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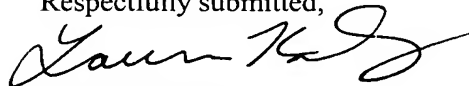
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Sir:

The above-identified application is being filed on behalf of the inventor, **Orlin Velev**, a citizen of Bulgaria, residing at 116 Rushingwater Drive, Cary, North Carolina, under the provisions of 37 CFR 1.41(c). A Declaration and Power of Attorney from the inventor will follow, 37 CFR 1.63.

Respectfully submitted,



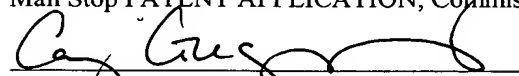
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Carey Gregory

## **DROPLET TRANSPORTATION DEVICES AND METHODS HAVING A FLUID SURFACE**

### **RELATED APPLICATIONS**

This application claims priority to United States Patent Application No. 60/439,624  
filed January 13, 2003, the disclosure of which is incorporated herein by reference in its  
5 entirety.

### **BACKGROUND OF THE INVENTION**

#### **1. Field of the Invention**

The present invention relates to methods and devices for the transportation of droplets  
10 or particles using an electric field gradient.

#### **2. Background**

The scaling down of chemical reactions, separations, and analysis processing using  
microfluidic devices may be useful in various areas of chemical engineering,  
15 pharmaceuticals, and biotechnology. Many of the microfluidic devices operate by  
microchannels inside plastic or glass, which can lead to surface fouling and other problems.  
The fluids of interest may be in direct contact with the plastic or glass. The liquid inside  
these channels generally flows in a continuous stream because high capillary pressures  
generated at any air-liquid boundaries in the microchannels may disrupt operation. Pumping  
20 and valving in such small channels may require a significant amount of energy because of  
high viscous dissipation. Therefore, many of these devices operate as continuous process  
devices.

Alternatives to continuous streams in microchannels include methods to move a liquid  
as a micro- or nano-droplet(s) using electric fields or gradients in interfacial tensions. The  
25 manipulation of microscopic droplets on a solid surface, however, may be technically  
difficult. For example, the contact angle hysteresis of the droplets can lead to strong capillary  
forces, which may increase losses of power and may pin the droplets onto surface  
contaminants and/or scratches. The open surface of the droplets, combined with the high  
capillary pressure in the droplets, may lead to rapid evaporation and/or surface fowling. In  
30 addition, molecular, particulate, or biological species inside the droplets can become  
adsorbed on the surface of the solid, which can lead to a loss of the component for which

processing is desired, higher contact angle hysteresis and chip contamination that can be difficult to reverse.

The manipulation of microdroplets can also be based on the application of alternating current ("AC") electric fields, called dielectrophoresis ("DEP"). DEP may be used for the manipulation, separation, and collection of cells, viruses, biomolecules and nanoparticles. AC voltages may be used to pull water droplets into a gap between liquid siphons, and similar techniques may be used to move water droplets on solid surfaces. T.B. Jones, M. Gunji, M. Washizu and M.J. Feldman, *J. Appl. Phys.* **89**, 14A-F41-14A-F48 (2001) *Dielectrophoretic liquid actuation and nanodroplet formation.*; T.B. Jones, *Electrostat.* **51**, 290-299(2001) *Liquid dielectrophoresis on the microscale.*; M. Washizu, *IEEE T. Ind. Applic.* **34**, 732-737 (1998). *Electrostatic actuation of liquid droplets for microreactor applications.*; M.G. Pollack, R.B. Fair, A.D. Shenderov, *Appl. Phys. Lett.* **77**, 1725-1726 (2000) *Electrowetting-based actuation of liquid droplets for microfluidic applications.* Parallel electrodes can be used that operate directly on water droplets that are placed on a solid surface. The droplets can be drawn between the electrodes because of the high dielectric permittivity of water. Relatively high voltages and/or high frequencies may be required, which can lead to significant power dissipation, heating of the aqueous phase, and evaporation. In addition, the droplets are generally in direct contact with a solid surface, such as plastic or glass. Thus, many of the problems discussed above with respect to surface fouling, evaporation, chip contamination, etc. may also be present.

#### SUMMARY OF THE INVENTION

In some embodiments according to the present invention devices are provided for the manipulation of a suspended particle in an electric field gradient. A plurality of electrically isolated electrodes are positioned on a surface. A liquid composition is on the plurality of electrodes. The liquid composition covers the surface continuously between adjacent ones of the plurality of electrodes. The liquid composition has an exposed liquid surface for suspending a particle. The plurality of electrodes are configured to provide an electric field gradient for transporting the particle suspended in said liquid composition.

In this configuration, particles, such as droplets, can be transported without contacting solid surfaces. Surface fouling, evaporation, chip contamination, power dissipation, and heating can be reduced.

Further embodiments according to the present invention provide methods for the manipulation of a suspended particle in an electric field gradient. A plurality of electrodes

are configured on a surface to provide an electric field gradient for transporting a particle. A liquid composition is applied on the plurality of electrodes. The liquid composition has an exposed liquid surface for suspending a particle. The particle is suspended in the liquid composition. A voltage is applied between selected ones of the plurality of electrodes to provide the electric field gradient. The electric field gradient defines a pathway for transporting the particle.

### BRIEF DESCRIPTION OF THE DRAWINGS

**Figure 1A** is a perspective schematic drawing of an electrode series for manipulating droplets on a substrate according to embodiments of the present invention.

**Figures 1B-1C** are side views of electric fields with gradients produced by electrodes submerged in a fluid having a droplet suspended therein according to embodiments of the present invention.

**Figures 1D-1H** are top views of electrode configurations according to embodiments of the present invention.

**Figures 2A-2B** are top views of equilibrium positions of 750nL droplets on an electrode array according to embodiments of the present invention.

**Figure 2C** is a colloidal crystal formed on the upper surface of a droplet according to embodiments of the present invention.

**Figure 2D** is a confocal microscopy three-dimensional reconstruction of a droplet containing 0.2 wt. % fluorescent latex where nearly all of the particles are concentrated on the droplet top surface according to embodiments of the present invention.

**Figures 3A-C** are top views of two droplets (**Figure 3A**) that are combined and mixed (**Figures 3B-C**) on a fluid-fluid electrode chip according to embodiments of the present invention.

**Figure 3D** is a micrograph of the combined droplet that results after two droplets containing polystyrene (white) and magnetic (brown) latex have been mixed to temporarily form anisotropic polymer aggregate according to embodiments of the present invention.

**Figure 3E** is a micrograph of a crystalline shell of calcium phosphate precipitated after mixing droplets containing solutions of  $\text{Na}_2\text{HPO}_4$  and  $\text{CaCl}_2$ .

**Figure 3F** is a micrograph of a water droplet containing 1.0 wt. % latex and 1.9 nM Na-dodecyl sulfate encapsulated inside a liquid dodecane shell.

**Figure 4** is a schematic drawing of an exemplary design of electrodes and their connecting leads in a fluid-fluid chip according to embodiments of the present invention.



treatment with respect to smoothness, wetting, etc. Although embodiments of the present invention are described herein with reference to droplets, it should be understood that solid particles can also be suspended in a fluid surface (e.g., fluid 16). Solid particles can result from precipitations of liquid droplets on the fluid surface, or solid particles can be deposited directly on the fluid surface. Liquid droplets of various viscosities can also be transported on a fluid surface. Moreover, the droplets can include other components, such as nanoparticles, microparticles, surfactants, protein, cells, viruses, polymers, polymerizable monomers, surfactants, silicone compounds, and/or combinations thereof. Such components can be included in the droplets 12 in any form by which the component can be carried, such as in solutions, suspensions, dispersions, micro-emulsions, emulsions, etc. The droplets 12 can be between about 0.01  $\mu$ L and about 10  $\mu$ L.

As shown in **Figure 1**, the suspended droplets 12 can be driven by alternating currents (AC) and/or direct currents (DC) applied to the electrodes 14A-F. Alternating current can be provided at between about 50V and about 500 V at a frequency between about 50 Hz and about 500 Hz. Exemplary ranges of DC voltages are between about 20 V And about 500V. The electrodes 14A-F are arranged in series and are electrically isolated from one another by the substrate 17. The electric field patterns created by the electrodes 14A-F allow controlled droplet motion along predetermined pathways. The electrodes 14A-F can be individually addressable by a controller, and typically, the electrodes 14A-F that are not switched to the high voltage source are grounded.

As described in more detail below, movement of multiple droplets can be controlled using electrodes, such as the electrodes 14A-F in **Figure 1A**, that provide an electric field gradient along one or more pathways. In some embodiments, the electrodes can be configured to provide two or more pathways that may intersect to combine droplets. Droplets can be combined on a single pathway by transporting droplets in opposite directions or in arbitrary directions on electrode arrays. Combined droplets can be used to provide various types of microassays, including assays known to those of skill in the art. For example, bioassays can be provided, which include microsphere agglutination or fluorescence assays for proteins DNA, RNA, viruses or other biologically specific markers. As another example, viability assays can be used to detect the viability status of cells, bacteria or viruses in droplets by mixing a droplet containing the cell, bacteria, or virus of interest with a droplet containing a toxin, virus, protein, or other disease-causing agent. Drug screening microassays may involve determining the viability status of cells, bacteria or viruses after mixing a droplet containing the cell, bacteria, or virus with a droplet(s) containing the drug

and/or a disease-causing agent. Chemical microassays can be performed such that the status of a certain chemical reaction is expressed by a change in color, precipitation, opalescence, or fluorescence after two droplets are mixed. Assays according to embodiments of the present invention can be used to detect toxins, chemical agents, environmental contaminants, detergency actions, etc. Mixing, drying or polymerization reactions can lead to the synthesis of advanced materials in the form of anisotropic or otherwise organized particles. Examples of such preparation and application of droplets and/or particles are given in O.D. Velev, K. Furusawa, K. Nagayama, *Langmuir* **12**, 2374 (1996); O.D. Velev and K. Nagayama, *Langmuir* **13**, 1856 (1997); O.D. Velev, A.M. Lenhoff, E.W. Kaler, *Science* **287**, 2240-2243 (2000), the disclosures of which are hereby incorporated by reference in their entireties.

Electrodes according to embodiments of the present invention can be configured in various shapes and positioned in various arrays to provide a desired electric field to manipulate motion of a droplet. Without wishing to be bound by any particular theory, in some embodiments, the application of a spatially inhomogeneous AC on electrodes can provide a dielectrophoretic (DEP) force,  $F_{DEP}$ , which acts in the direction of the gradient of the squared electric field,  $\Delta E^2$ , and which can be described by the following equation.

$$\vec{F}_{DEP} = 2\pi\epsilon_1 \text{Re}[K(w)]r^3 \Delta E^2$$

where  $r$  is the radius of the particle (e.g., the droplet **12** in **Figure 1A**),  $\epsilon_1$  is the dielectric permittivity of the media (e.g., the fluid **16**), and  $K$  is the Clausius-Mossotti factor. The direction and magnitude of the DEP force depend on the real part of  $K$ , which in the example given in **Figure 1A** is the effective polarizability of the droplet **12** and is generally higher than droplets in a continuous liquid media, such as in microchannel devices. The droplets **12** can also be attracted and repelled by constant DC fields applied to the electrodes **14A-f**. The forces operating in this case include common electrostatic (Coulombic) attraction and repulsion. These forces are possible because the droplets possess charge, and/or dipole moment.

The equilibrium position of one of the droplets **12** with respect to the electrodes depend on the pattern and/or frequency of the voltage on the electrodes **14A-F**. As shown in **Figure 1A**, electrodes **14A**, **14C**, **14D**, and **14F** are grounded, and electrodes **14B** and **14E** are provided with AC power. Further examples of electrodes and electrode field gradients are shown in **Figures 1B-1C**, in which electrodes **24A-24D**, **34A-34D** are submerged in fluids **26**, **36**, respectively. The fluids **26**, **36** each have an exposed surface **26A**, **36A** in contact with surrounding air **20**, **30**. Droplets **22**, **32** are suspended in the fluids **26**, **36** and

manipulated by the electric field gradients provided by the electrodes **24A-24D**, **34A-34D**. Electrodes **24C**, **24D**, **34A**, **34C**, and **34E** are grounded, and electrodes **24A**, **24B**, and **34B** are connected to an AC power source. In **Figures 1A-C**, the droplets **12**, **22**, **32** can be water droplets and the fluids **16**, **26**, **36** can be perfluorinated hydrocarbon oil (F-oil). Water droplets can be attracted along the electric field gradient produced by the electrodes **14A-F**, **24A-D**, **34A-D** to regions of high field intensities because water droplets have a higher dielectric permittivity and conductance than F-oil.

For example, as shown in **Figure 1B**, the electrodes **24A-24D** are connected in sequences of two energized electrodes **24A**, **24B** and two grounded electrodes **24C**, **24D**. The droplet **22** migrates to the gap between the energized electrodes **24A**, **24B** and the non-energized electrodes **24C**, **24D** because the droplet position at this gap is in close proximity to the area of highest field intensity. On the other hand, if a single energized electrode is positioned between grounded electrodes, the electric field gradients can position the droplet substantially above the energized electrodes. As shown in **Figure 1A**, the droplets **12** are positioned above the energized electrodes **14B**, **14E**, and in **Figure 1C**, the droplet **32** is positioned above the energized electrode **34B**. The trapped droplets **12**, **32** can be moved by consecutively switching on and off the voltage to the various electrodes **14A-14F**, **34A-34D**.

Electrodes according to embodiments of the present invention can be shaped in various configurations. For example, the electrodes can be conductive rings having an interior void, such as the circular ring electrodes **40** shown in **Figure 1D** or the square ring electrodes **42** shown in **Figure 1E**. Pairs of electrodes can also be used to provide a desired electric field gradient, such as the "herringbone" configuration of electrode pairs **44A**, **44B** shown in **Figure 1F**. The electrodes can be arranged in an array to provide pathways along which a droplet can be transported. For example, in **Figure 1G**, electrodes **46A** define one pathway and electrodes **46B** define another pathway. Electrodes **46D** define still another pathway. The electrode pathways intersect at electrode **46C**. The configuration shown in **Figure 1G** can be used to combine or divide one or more droplets. For example, droplets transported along electrodes **46A** from left to right and droplets transported along electrodes **46B** from left to right can be combined with one another at the intersection electrode **46C**. On the other hand, the voltages applied to the electrodes **46A-D** can be selected such that droplets can be transported along electrodes **46** from right to left and separated into two droplets at intersection electrode **46C**. One of the resulting droplets is transported away from electrode **46C** along electrodes **46A**, and the other droplet is transported away from electrode **46C** along electrodes **46B**. As another example of an electrode configuration that can be



used to combine droplets with reference to **Figure H**, electrode pairs **48A, 48B, 50A, 50B, 52A, 52B** can be used to combine one droplet **54A** from electrode pair **48A, 48B** with another droplet **54B** from electrode pair **50A, 50B**. The combined droplet **54C** can be further transported by an additional electrode pair **52A, 52B**. The electrodes can also be combined in a two-dimensional array so that a droplet can be moved in horizontal, vertical, or diagonal directions, depending on which of the surrounding electrodes are energized by the controller.

In some embodiments, the electrodes described in the examples above can have a length of between about 0.1 mm and about 1 mm and a distance between electrodes in a given array of between about 0.1 mm and about 1 mm.

The following non-limiting examples are provided to illustrate various embodiments according to the present invention in detail.

### **Example 1**

#### **Fluid-Fluid Droplet Transport Devices**

Electrodes and electrical leads were fabricated on two-sided printed circuit boards that have electrodes on one side and connecting leads on the other. An exemplary device **70** is shown in **Figure 4**. An array of electrodes **78** is arranged on a circuit board substrate (not shown). The electrodes **78** are connected to a controller **74** by leads **76, 76A, 76B**. As illustrated, the leads **76A** pass above the circuit board and leads **76B** (dashed lines) pass below the circuit board. A controller **74** that includes a power source **72** controls power to the electrodes **78**. The power source **72** can be an AC and/or a DC power source. The controller **74** can also include a computer controlled switch box, and amplifier, and/or a signal generator for controlling the signals to the electrodes **78**.

The electrode boards were immersed inside 50 mm Petri dishes filed with perfluoromethyldecaline (PFMD). The electrode leads were connected through a computer controlled switch box to an amplifier a signal generator. Electrodes that were not switched to a high voltage amplifier output were grounded. The transition between AC to DC signals could be made gradually by varying the symmetry ratio of the AC waves, from full negative, to symmetric AC, to full positive voltage. Some droplets were formed from aqueous suspensions of polystyrene latex microspheres that were purchased from Interfacial Dynamics Corp. (OR). Other droplets contained gold nanoparticle suspensions that were synthesized by citrate reduction of auric acid in the presence of tannic acid.

As shown in **Figures 2A-D** and **3A-D**, droplets were suspended in the PFMD oil of a device as describe above and transported by AC and/or DC currents applied to the arrays of

individually addressable electrodes. The droplets included water or dodecane droplets having a volume of about 500-100 nL, which were formed by micropipette and suspended at the oil/air interface without contact with the electrodes. Some of the water droplets used contained suspensions of micro- and nanoparticles as described above. The droplets were driven with AC or DC voltages in the range of 200-600 V. The AC frequencies were in the rang of 50-5000 Hz.

**Figure 2A** illustrates the initial equilibrium positions of four droplets **50A-D** on an array of electrodes **52**. Every fourth electrode beginning from the left side of the picture is energized. The droplets **50A-D** contain fluorescent latex microparticles (droplet **50A**), gold nanoparticles (droplet **50B**), white latex (droplet **50C**), and magnetic latex (droplet **50D**). **Figure 2B** illustrates another position of the droplets after three cycles of switching the electrodes **52** to the right. The scale bar **54** is 1 mm.

As illustrated, multiple droplets containing different nano-particles (or other components), can be transported on chips with a large number of individually addressable electrodes. The droplets can be directed along the desired track by switching electrodes, and electric field gradients can be configured to combine or separate the droplets. The two-dimensional matrixes of individually addressable electrodes can allow independent positioning, movement in a desired direction, mixing of droplets of various compositions, and/or the separation of a droplet into two droplets.

## Example 2

### Parameter Effects

The effects of basic system parameters on droplet mobility in the devices described in **Example 1** are summarized in Table 1 below.

**Table 1.** Effect of the experimental parameters on the responsiveness and mobility of the suspended microdroplets.

Factor	Range studied	Effect on droplet responsiveness
AC field	Symmetric square waves	Moves water droplets towards areas of highest field intensity ( <b>Fig. 1A-B</b> ).
DC bias	0 - 500 V	Attraction or repulsion, followed by re-charging. Moves both water and oil

		droplets. Very strong, but erratic.
AC amplitude	0 - 600 V	Increases ( $\uparrow$ ) proportionally to $E^2$
AC frequency	50 - 5000 Hz	None
Droplet volume	500 - 1500 nL	$\uparrow$
Distance between droplet bottom and chip surface	0.01 - 0.5 mm	Decreases ( $\downarrow$ )
Electrolyte in water droplets	None added - 0.1 M	( $\uparrow$ ) Small
Fluorinated or non-fluorinated surfactant added in droplet	0 - 0.1 wt. %	None
Full immersion of the droplets in overlying dodecane layer	-	$\downarrow\downarrow$ Could lead to complete loss of responsiveness
Electrode geometry	Square or circular	Square electrodes more effective at shorter drop-electrode distance, circular at larger

### Example 3

#### Particle Crystallization

Internal polarization of droplets, such as the droplets described in **Example 1**, may be evidenced by observing the vertical distribution of particles contained inside the droplets. Negatively charged latex microparticles inside a droplet can migrate and accumulate on the side of the droplet cap that protrudes above the fluid in which the droplet is suspended. Color diffraction from the concentrated particle phase directly below the droplet surface may be observed, which may indicate that the particles on top can become concentrated to the point of colloidal crystallization. **Figure 2C** illustrates colloidal crystals formed on the upper surface of a droplet containing 20 wt. % of sulfate latex. The droplet is suspended in oil, and the upper surface of the droplet is exposed to air above the oil/air interface. The particles have crystallized because of attraction to the top surface. **Figure 2D** is a confocal microscopy three-dimensional reconstruction from above the droplet in **Figure 2C**

illustrating that nearly all of the particles are concentrated at the top surface. The scale bar 56 is 500  $\mu\text{m}$ .

The asymmetric dielectric environment can provide this polarization of particle distribution. In contrast, when a thick layer of dodecane was poured on top of the perfluorinated hydrocarbon oil so that the droplets were immersed in a media with uniform dielectric constant, the particles remained essentially uniformly dispersed. The concentration of particles at the upper surface of a droplet may be used in droplets that are carriers for micro- and nanoparticles and living cells because it allows their contents to be thus separated and clearly visible on the top side of the droplet.

#### Example 4

##### Droplet Mixing

Figures 3A-C illustrate the mixing, precipitation, and encapsulation in aqueous microdroplets suspended on a matrix fluidic chip. An electrode array 68A is submerged in oil as described in Example 1. A droplet 62 containing magnetic latex and a droplet 64 containing polystyrene are suspended in the oil in Figure 3A. As shown in Figure 3A, the droplets 62, 64 are transported along two respective pathways and combined at an intersection between the pathways to form a combined droplet 66. The combined droplet 66 can be further transported as shown in Figure 3C.

A two-dimensional matrix electrode array 68B having a droplet 62B thereon is shown in Figure 3D. The electrodes of the two-dimensional matrix array 68B are spaced such that a droplet can be moved vertically, horizontally, and/or diagonally. The electrode array 68B has been submerged in oil as described in Example 1. As illustrated, the droplet 62B is the result of a combination of a droplet containing polystyrene (white) and another droplet containing magnetic (brown) to temporarily form an anisotropic polymer aggregate. That is, when particles carried inside droplets were allowed to segregate to the top of the droplet prior to mixing, intermittent anisotropic clusters of particles formed on the surface of the newly combined particle 62B, as shown in Figure 3D. Because fluidic chips according to embodiments of the invention can provide massive parallelization, such chips can be used for automated fabrication of functional micro- and nano-assemblies, such as "supraparticles" with colloidal crystal structure. The scale bar 60A is 1 mm.

#### Example 5

##### Droplet Mixing and Precipitation

A variety of mixing and precipitation experiments were performed by controllably merging pairs of droplets of different compositions, such as those described with respect to **Figures 3A-D** on a chip as described in **Example 1**. The complex precipitation patterns inside the mixed droplets can lead to the formation of crystal shell-like balls. These particles have a water core inside and could be further moved intact along the electrodes. Such shell-like crystalline particles may be used, *e.g.*, as biomimetic capsules. **Figure 3E** shows a crystalline shell of calcium phosphate precipitated after mixing droplets containing solutions of  $\text{Na}_2\text{HPO}_4$  and  $\text{CaCl}_2$ . The scale bar **60B** is 1 mm.

Water and hydrocarbon droplets on the chips were combined in a 1:1 ratio. The droplets can be mixed as described with respect to droplets **62, 64** in **Figures 3A-C**. When a surfactant, such as sodium dodecyl sulfate, was added to the water droplets, the interfacial tensions balance can favor the complete engulfment of the water droplet in the hydrocarbon droplet. The water droplets became symmetrically encapsulated inside a liquid hydrocarbon shell. **Figure 3F** illustrates a water droplet containing 1.0 wt. % latex and 1.9 mM Na-dodecyl sulfate encapsulated inside a liquid dodecane shell. The scale bar **60C** is 1 mm.

## Example 6

### Power Dissipation

The devices and methods described in **Examples 1-5** were used to transport various droplets using various electrode patterns. The maximum speed at which droplets can be moved by switching AC power to the electrodes may be approximately proportional to  $E^2$ , as provided by the above formula for  $F_{DEP}$ , which was verified experimentally. Power dissipation (also verified experimentally) may be relatively low because the currents through the electrode may be smaller than the capacitance leaks in the circuit. It has been estimated that the energy needed to transport a suspended droplet in some embodiments of the invention can be on the order of  $1 \times 10^{-9}$  J/cm for droplets having a volume of between about 500 and 1000 nL. In contrast, the energy required to move a similar droplet size on a solid surface or in microfluidic channels may be two orders of magnitude greater.

A liquid-liquid microfluidic chip as described in **Example 1** was prepared. An estimate for the energy required to move a 500nL water droplet 1 cm at 2 mm/s using the chip as described in **Example 1** is compared to estimates for energies for transporting similar droplets by conventional microfluidics with channels in Table 2.

**Table 2**

	Droplet moved in F-oil	Hemispherical droplet dragged on solid surface	Viscous flow in microfluidic channel
Assumptions and approximations	<ul style="list-style-type: none"> <li>Stokes sphere in bulk liquid</li> </ul>	<ul style="list-style-type: none"> <li><math>\theta_{Advancing} = 90 \text{ deg}</math></li> <li><math>\theta_{Receding} = 80 \text{ deg}</math></li> <li>No viscous dissipation</li> </ul>	<ul style="list-style-type: none"> <li>Circular channel of diameter <math>20 \text{ }\mu\text{m}</math></li> <li>Poiseuille flow</li> </ul>
Type of estimation	Overestimate	Underestimate	Underestimate
Energy required / J	$\leq 9.4 \times 10^{-10}$	$\geq 1.6 \times 10^{-7}$	$\geq 1.4 \times 10^{-4}$
Energy ratio	1	170	150000

### Example 7

#### Electric Fields and Energy

5 Various electric fields can be provided to obtain the desired movement of droplets. For example, AC power can be used as discussed above or droplets can also be transported using a DC power source to provide constant electrical voltages. Water droplets may respond strongly to DC fields by either moving rapidly away from an energized DC electrode, or by being strongly attracted towards it. The velocity of droplet motion and the range of the interactions may be larger than the AC-driven effects at the same voltage range. For example, the velocity can be twice as large and reach speeds of 2.0 mm/s or higher. This speed may be due to the water droplets having a significant charge and/or dipole moments that respond to Coulombic repulsion or attraction. The sign of the charge of a droplet made from various suspensions can vary from positive to negative. The droplets may be charged by collecting static charges from the interface of the fluid in which the droplet is suspended and/or from a charge transfer through the fluid phase. Furthermore, charging and/or re-charging effects may be observed at combined AC+DC voltages. The use of DC fields can be used to manipulate other droplets, such as hydrocarbon oil droplets. These droplets may not respond to symmetric AC fields due to a lack of polarizability because their dielectric permittivity is close to that of PFMD. However, hydrocarbon oil droplets may respond to a constant field in a manner similar to water droplets.

### Example 8

#### Droplet Velocity

25 The speed of a droplet placed on devices described in **Example 1** was measured. The droplet was a 750 nL aqueous droplet submersed in a 1.15 mm deep PFMD layer. The speed

was measured by the shortest time required for the droplet to traverse an automated eight electrode sequence in a forwards and backwards direction. The field was estimated by dividing the voltage applied by the electrode pitch, which was 1.54 mm. The AC frequency was 200 Hz. The droplet speed as a function of the field intensity squared is shown in **Figure**

5 **5.**

Embodiments of the present invention described herein can be combined with existing electrowetting and channel microfluidics techniques in larger integrated devices. This can be used for automatic droplet dispensing onto the fluorinated oil surface. For example, the existing techniques for droplet breakup and manipulation by electrowetting on solid surfaces  
10 [see, e.g., T.B. Jones, M. Gunji, M. Washizu and M.J. Feldman, *J. Appl. Phys.* **89**, 14A-F41-14A-F48 (2001) *Dielectrophoretic liquid actuation and nanodroplet formation.*] could be used to break up droplets from a larger volume of liquid at the edge of the chip. This can automate the procedure of droplet deposition on the surface of the liquid, which may also be done by a micropipette. Droplets can then be further manipulated as described herein.  
15 Similarly, common microfluidic channels can be used for liquid transport to a chip and droplet breakup. The removal of droplets from liquid surfaces and their collection and/or disposal can also be performed by using electrowetting or microfluidic channels.

In the drawings and specification, there have been disclosed typical embodiments of the invention and, although specific terms are employed, they are used in a generic and  
20 descriptive sense only and not for purposes of limitation, the scope of the invention being set forth in the following claims.